



Outline

- Overview Status & Plans (R. Petre)
- Mirror Segment Fabrication (W. Zhang)
- Alignment and X-ray Test Preparations (S. Owens)



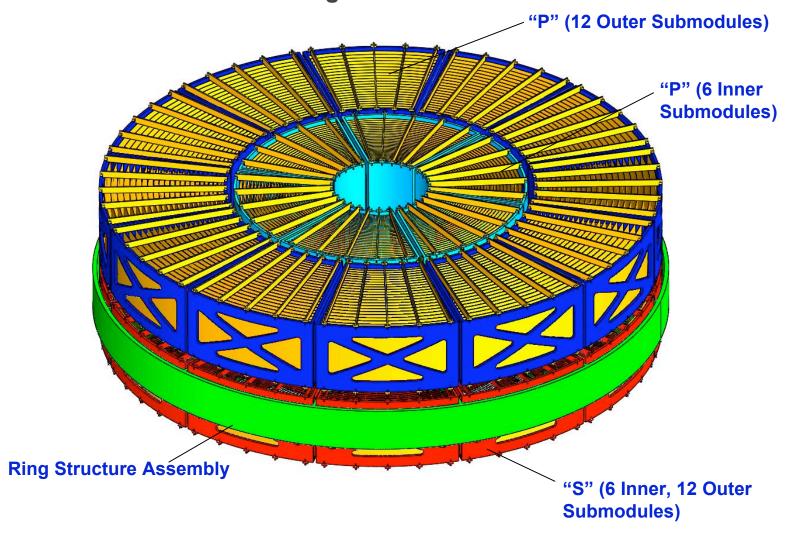
SXT Flight Mirror Assembly Requirements (per mirror)

| SXT FMA Performance Requirements | | Trace to Top-Level Mission Requirements | | | |
|---|---|--|--|--|--|
| Bandpass | 0.25 to 10 keV | Allocation of mission bandpass to SXT | | | |
| Effective area allocation @0.25 keV @1.25 keV @6 keV | 7,025 cm ² 6,797 cm ² 1,830 cm ² | Includes estimates for structural blockage and optical losses. Allocation changed from TRIP due to higher throughput from off-plane gratings, providing more margin on effective area of the telescope system | | | |
| Angular resolution | 12.5 arcsec HPD | Error budget allocation to mirror that allows telescope system to achieve requirement of 15 arcsec with 4 arcsec margin combined by RSS. | | | |
| Field of view | 2.5 arcmin | Defined by detector field of view (FOV) | | | |
| Derived Requirements: SXT Mirror | | Derivation | | | |
| Diameter | 1.6 m | To meet mission area requirements with 4 mirrors | | | |
| Focal length | 10 m. | Consistent with grazing angle requirements for 1.6 m diameter mirror. | | | |
| Axial length | <70 cm | To fit within envelope and meet fabrication considerations | | | |
| Operating temperature | 20±1° C nominal | Range is per allocation from SXT angular resolution error budget; minimiz angular distortions imposed by temperature change to components. Operating temperature is determined by optics assembly temperature | | | |
| Mass | 642 kg | Allocation (includes thermal collimators) | | | |



SXT Mirror Reference Concept

General Overview of Design



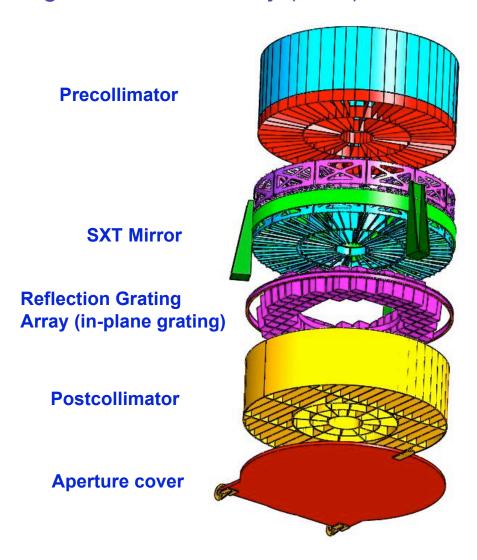


SXT Mirror Reference Design Parameters

| Parameter | Description | | | |
|-------------------------------|--|--|--|--|
| Design | Segmented Wolter I | | | |
| Segment substrate material | Thermally formed glass | | | |
| X-ray reflecting surface | Gold | | | |
| Number of nested shells | 127 (inner); 89 (outer) | | | |
| Total number of segments | 3660 | | | |
| Mirror segment length | 20 cm | | | |
| Number of modules | 6 (inner); 12 (outer) | | | |
| Module housing composition | Titanium alloy, CTE-matched to substrate | | | |
| Module support structure | Composite | | | |
| Largest segment surface area | 0.08 m ² | | | |
| Substrate density | 2.5 gm/cm ³ | | | |
| Mirror segment thickness | 0.44 ± 0.02 mm | | | |
| Mirror segment microroughness | 6 Angstroms RMS | | | |
| FMA mechanical envelope | 1.68 m dia x 1.98 m | | | |



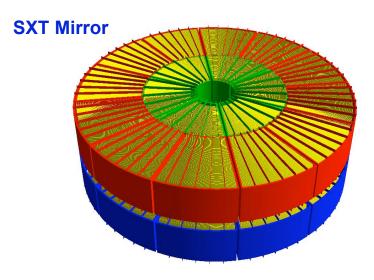
SXT Flight Mirror Assembly (FMA)



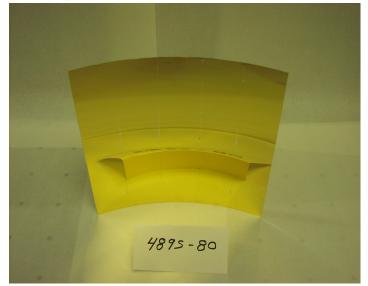


Elements of SXT Mirror Technology

- Mirror segment fabrication process
 - Thin, thermally formed glass substrates with gold overcoat
- Precision-figured mandrel fabrication and metrology
 - Forming and replication mandrels
 - Cylindrical and slab mandrels
- Metrology for light-weight mirror segments
 - Perform metrology with minimum distortion to segments



Mirror Segment

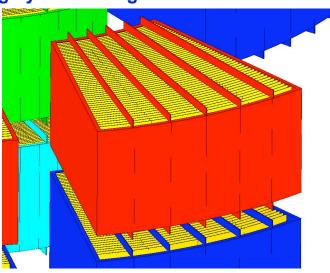




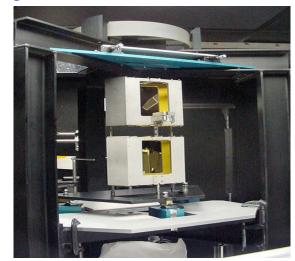
Elements of SXT Mirror Technology (cont.)

- Alignment tools and techniques
 - Non-rigid body alignment with minimum figure error distortions
 - Mass alignment of multiple mirror pairs
- Mirror mounting and structural support
 - Minimum distortions to mirror segments
 - Facilitate alignment
- Mechanical properties of mirror segments
 - Mirror substrate (glass) strength
 - Glass thermal properties
 - Bonding to housing
- Technology must be transferable to industry for flight production

Highly nested segments



Alignment





Technology Development Roadmap Summary

| | Optical Assem | nbly Pathfinder | Mass Alignment | Engineering | Subassembly | |
|---------------------------------------|--|---|--|---|--|--|
| | OAP #1 | OAP #2 | Pathfinder | Unit | | |
| Configuration | P | PH | P | P | | |
| Module Type | Inner | Inner | Inner | Two inner modules | NASA Testbed – Outer + Inner | Industry Prototype – Outer + Inner |
| Housing Material | Aluminum | Titanium | Titanium | Titanium | Titanium | Titanium |
| Focal Length | 8.4 m | 8.4 m | 8.4 m | 10 m or 8.4 m (TBD) | 10.0 m | 10.0 m |
| Nominal mirror segment Diameter(s) | 50 cm | 50 cm | 50 cm± | 50 cm± | 160 cm 120 cm± 100 cm, 50 cm± | 160 cm± 120 cm± 100 cm±, 50 cm± |
| Goals | Align 1 mirror segment pair (P&H) Evaluate mirror assembly design, alignment and metrology | Align 1 mirror segment pair Evaluate segment performance and stability in mount Evaluate mirror bonding X-ray test Vibration test | Align up to 3 mirror segment pairs to achieve <12.5 arcsec Evaluate tooling for mass alignment Vibration & X-ray tests | Fabricate segments from slab mandrels Align module to module. X-ray and environmental tests Technology transfer to industry Evaluate assy gravity sag | Form largest mirror segments Demonstrate reference subassembly design Environmental and X-ray test | Demonstrate flight prototype Environmental and X-ray test Industry build |
| TRL - Mirror segment | TRL 3 | TRL 4/5 | | TRL 6 | | |
| TRL - Assembly | TRL 3 | TRL 3/4 | TRL 5 | TRL 6 | | |
| Timeframe | Q2 of FY03 | Q2 of FY06 | | 2 | 006 - 2009 | |
| Technology Gate | | | u | | u | |



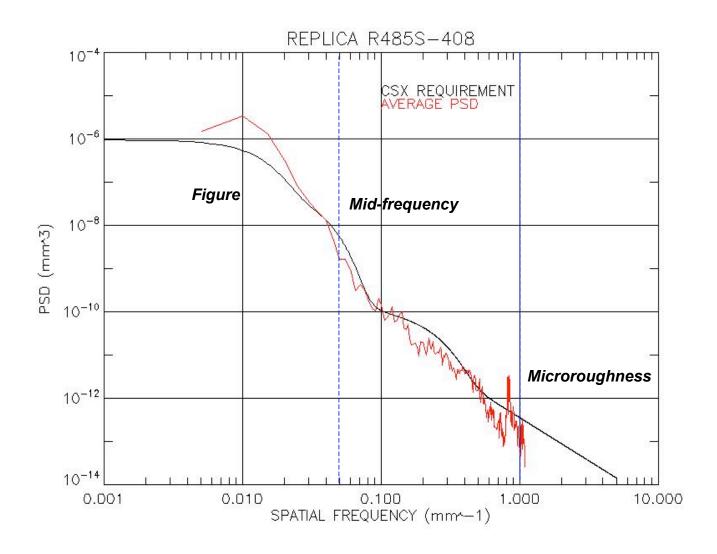
Mirror Segments - Technical challenges

We have a clear understanding of elements of producing mirror segments

- Three largely decoupled spatial frequency domains
 - Low order 2-20 cm
 - Mid-frequency 0.1-2 cm
 - High-frequency (microroughness) <0.1 cm
- Low order
 - Determined by forming; not improved by replication
 - Distortions due to gravity, mechanical stresses appear in this regime
 - Dictate forming mandrel requirements
- Mid frequency
 - Imparted to substrate during forming
 - Very sensitive dependence on physics of forming process
 - Very sensitive to presence of particulates
 - Corrected by epoxy replication
- Microroughness
 - Substrate material has excellent microroughness; preserved during forming
 - Replication introduces entirely new microsurface this places requirements on replication mandrel microroughness (superpolishing is necessary)



Spatial Frequency Domains





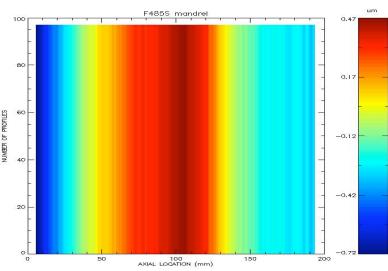
Mirror Segments - Recent Progress

- Demonstrated that formed substrates faithfully and consistently reproduce the forming mandrel surface at low spatial frequencies
- Improved the formed and replicated mirror quality by reduction of size and number of particulates (dust) on surface
 - Invested considerable effort reducing environmental dust in mirror lab
- Demonstrated that replication with ~10 µm epoxy layer can smooth out mid-frequency errors without causing significant distortion to low order figure
- Demonstrated feasibility of producing mirror segments meeting the error budget requirement without replication
 - Low and mid frequency improvement is likely if more precise forming mandrels are used
- Demonstrated that low order figure distortions are very sensitive to segment orientation and how it is held
- Developed a forming mandrel release layer that is very smooth and durable, and reduces mid-frequency roughness introduced by forming
 - Possible to apply using robotic spraying (developed for epoxy)
 - Process improvements still being sought

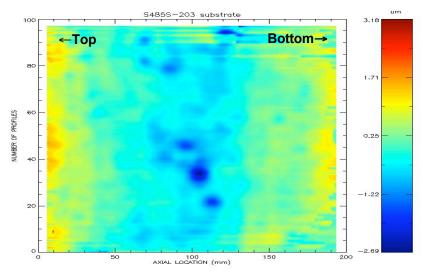


2D Contour plot of recent substrate

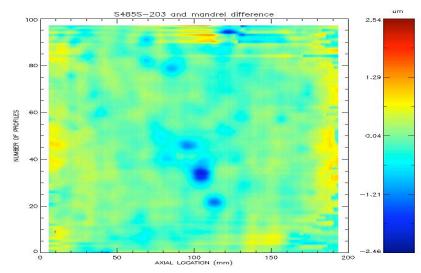
- 98 profiles measured; piston and tilt removed
- Single mandrel profile expanded to 2D
- RMS height error =0.30 μm
- Difference map represents <u>upper limit</u> of actual difference
- Large deviations due to dust particles
- Large deviation at top due to mounting fixture



1D profile of forming mandrel



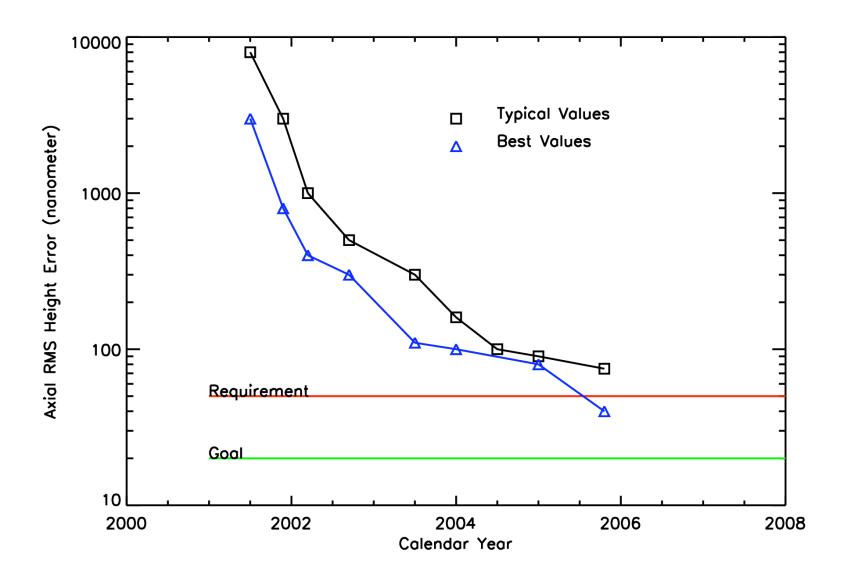
Measured profile (piston and tilt removed)



Difference between mandrel and substrate



Mirror Segment Figure Improvement





Mirror Segments - Challenges to Consistently Meeting Requirement

- Improvement of glass forming environment, including a clean/vacuum oven
- Better understanding of the surface physics of forming
- Ability to perform mechanical/thermal modeling of forming
- Improvement of the glass sheet cleaning process
- Better control of the epoxy replication environment: a mandrel coating chamber at GSFC
- Improved metrology of segment figure
 - Virtually impossible to measure free-standing segment, especially
 2nd order sag
 - Such measurements are largely irrelevant expect coupling between segment and mount (can't independently determine error budget terms)
 - We are building a 10-point mount to emulate conditions in housing, which facilitates 2D surface metrology



Mirror Segment Metrology Allocation vs. Measurement (ordered by HPD contribution)

| Parameters | Units | Allocation | Status | Instrumentation | Plan/Comments |
|--------------------|-------------|------------|--------|--------------------------|---|
| AXIAL FIGURE | | | | | |
| Slope | arcsec, rms | 0.75 | 0.35 | Interferometer | |
| Mid-frequency | nm, rms | 2.53 | 0.5 | Interferometer, Bauer200 | |
| Micro-roughness | nm, rms | 0.19 | 0.1 | Microinterferometer | |
| Sag | μm, pv | 0.04 | _ | Interferometer, MMTC | 10-point mount will improve accuracy. Plan for better thermal control. Gravity back out model & verification required. |
| Delta-delta-radius | arcsec, pv | 0.22 | _ | MMTC, Null lens | MMTC ∆∆R on mirror segment dominate by room thermal changes; Null lens needs permanent mount & calibration. |
| Roundness | μm, pv | 1.58 | 3.5 | MMTC | Dominated by room thermal changes (range during test from 2.7µm to 3.5 µm) Plan for better thermal control. |
| Cone-angle | arcsec | 3.16 | _ | MMTC | Optipro/MMTC. 10-point mount will improve accuracy. Plan for better thermal control. ±0.65 arcsec measured on solid calibration cylinder. |
| Average radius | _m | 10.4 | _ | MMTC | Optipro/MMTC. 10-point mount will improve accuracy. Plan for better thermal control. ±1.8 µm measured on solid calibration cylinder. |



Metrology - Recent Progress

- Demonstrated that Centroid Detector Assembly (CDA) designed for Chandra mirror alignment can be used to align mirror segments – purchased upgraded CDA
- Improved metrology techniques for measuring segments
 - Validated interferometric axial profiling technique
 - Confirmed optical microroughness metrology provides a precise prediction of mirror segment X-ray scattering
 - Designed and procured a cylindrical null lens for axial metrology over the full height by 2/3 width of segment
 - Obtained equipment to perform metrology with minimum distortions to segments
 - Introduced non-contact cylindrical Coordinate Measuring Machine (CMM) measures cone angle, radius, and low-order figure without touching the part
- Reduced the vibration sensitivity of measurements
 - Completed modeling and measurement to establish the need for vibration insensitive metrology and/or better mechanical isolation
 - Vibration robust, full-aperture interferometer is nearly ready for delivery
 - 10-point mount design reviewed and in work (will alleviate vibration & thermal drifts)

Plan for better lab environment control



Reference FMA Concept

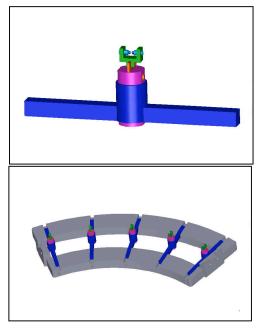
Typical Primary/Secondary (P/S) Module Stack up:

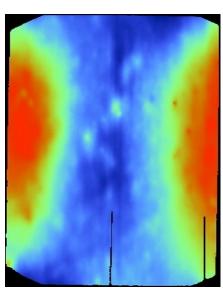
Typical Strut (5 Top, 5 bottom on each Submodule) This concept uses flexures to attach the P and S sub-modules together, as well as, to the Ring **Structure Assembly Typical Flexure Assembly 4 Places** HOUSING BUSHING (SHEAR CONNECTION IN TO HOUSING) BRACKET - P HOUSING - SCREW & WASHER EPOXY AROUND BUSHING CONICAL BUSHING (CUPS ARE MACHINED INTO P & H HOUSING BRACKET) **FLEXURE** H HOUSING SCREW & WASHER THROUGH FLEXURE BRACKET — H HOUSING RIB STRUCTURE BUSHING (SHEAR CONNECTION INTO HOUSING) P Submodule FMA Ring Structure Assembly AROUND BUSHING S Submodule ("Wagon Wheel") SECTION A-A

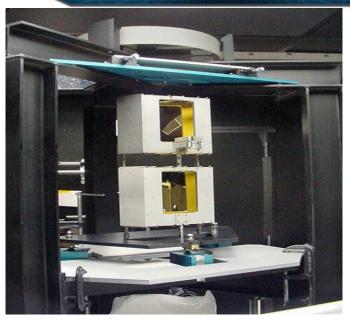


Segment Alignment

- Developed an alignment technique using CDA and in-situ interferometric monitoring of mirror figure
- Demonstrated the ability of piezoelectric bending actuators to align a single secondary mirror using CDA feedback
- CDA: RMS diameter of 4.35 arcsec in the focal plane based on 12 positions across the mirror segment
 - Developing alignment procedure

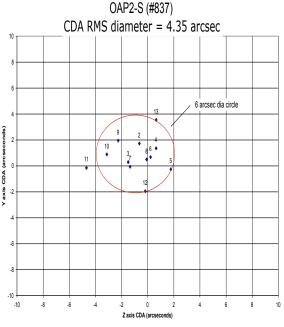






95 mm out of 200 mm height

27 deg out of 50 deg azimuth





Plans for Coming Year (and Beyond)

- Mount and align one or more pairs of mirror segments
 - Perform in situ full surface metrology within OAP2 mout
 - Demonstrate that aligned segments meet the Constellation-X HPD requirement
 - Quantify residual errors to determine most significant contributions
 - Compare 3D segment surface measurements and distortions (using special metrology mount) with optical and mechanical models
- Verify performance of aligned mirror pair(s) in X-rays; compare with predictions from metrology
- Continue development of alignment procedures
 - Introduce next generation Piezo actuators
 - Integrate collimated beam, surface profile interferometry, and CDA
- Refigure forming mandrel pair to allow 3 arc second HPD (Con-X goal)
- Procure and test 50 cm "slab" forming mandrel
 - Couple with thermo-mechanical modeling of forming process
 - Initiate conversion of forming to "flight-like" mandrels
- Involve industry in studies of Flight Mirror Assembly and mandrel fabrication
 - Mandrel fabrication is critical path of the program need to identify multiple suppliers
 - Mounting process could benefit from independent engineering study
- Support project efforts to reconfigure Con-X and approach performance goals
- New funding reductions will significantly delay all mirror technology development, and could result in irretrievable loss of knowledge



Summary

- The current forming technique produces substrates of consistent quality, approaching the Con-X requirement.
- Epoxy replication might not be necessary.
- Our knowledge of the mirror performance is limited by primarily metrology fixturing.
- The mirror performance is limited by mandrel quality and contamination
- We have means of performing all necessary diagnostic metrology of mirror substrates.
- We have a refined approach to aligning and mounting mirror segments, incorporating piezoelectric actuators and additional steps.
- Aligning a good segment pair to within the Con-X requirement should be possible using the current approach.